

31

1336

08/607169
10/1/77

- 1 -

CFO 11250 US

SCANNING OPTICAL APPARATUSBACKGROUND OF THE INVENTIONField of the Invention

5 This invention relates to a scanning optical apparatus and a multibeam scanning optical apparatus, and particularly to a scanning optical apparatus and a multibeam scanning optical apparatus suitable for use, for example, in an apparatus such as a laser beam

10 printer (LBP) or a digital copying apparatus having the electrophotographic process adapted to deflect and reflect a beam of light optically modulated and emitted from light source means by a light deflector (deflecting element) comprising a rotatable polygon

15 mirror or the like, thereafter optically scan a surface to be scanned through an imaging optical system having the $f\theta$ characteristic ($f\theta$ lens) and record image information.

Related Background Art

20 Heretofore, in the scanning optically apparatus of a laser beam printer or the like, a beam of light optically modulated and emerging from light source means in conformity with an image signal has been periodically deflected by a light deflector comprising,

25 for example, a rotatable polygon mirror and has been converged into a spot-like shape on the surface of a photosensitive recording medium (photosensitive drum)

having the $f\theta$ characteristic, and that surface has been optically scanned to thereby effect image recording.

Figure 1 of the accompanying drawings is a schematic view of the essential portions of a scanning optical apparatus according to the prior art.

In Figure 1, a divergent beam of light emitted from light source means 61 is made into a substantially parallel beam of light by a collimator lens 62, and the beam of light (the quantity of light) is limited by a stop 63 and enters a cylindrical lens 64 having predetermined refractive power only in a sub scanning direction. Of the parallel beam of light having entered the cylindrical lens 64, that part in a main scanning section intactly emerges in the state of a parallel beam of light. Also, that part in a sub scanning section converges and is imaged as a substantially linear image on the deflecting surface (reflecting surface) 65a of a light deflector 65 comprising a rotatable polygon mirror. Here, the main scanning section refers to a beam section the beam of light deflected and reflected by the deflecting surface of the light deflector forms with time. Also, the sub scanning section refers to a section containing the optical axis of an $f\theta$ lens and orthogonal to the main scanning section. The beam of light deflected and reflected by the deflecting surface 65a of the light deflector 65 is directed onto the surface of a

photosensitive drum 68 as a surface to be scanned through an imaging optical system ($f\theta$ lens) 66 having the $f\theta$ characteristic, and the light deflector 65 is rotated in the direction of arrow A to thereby
5 optically scan the surface of the photosensitive drum 68 and effect the recording of image information.

To effect the highly accurate recording of image information in a scanning optical apparatus of this kind, it is necessary that curvature of image field be
10 well corrected over the entire area of a surface to be scanned and a spot diameter be uniform and that the angle and image height of the incident light have distortion ($f\theta$ characteristic) in which they are in a proportional relation. A scanning optical apparatus
15 satisfying such optical characteristics or the correcting optical system ($f\theta$ lens) thereof has heretofore been variously proposed.

On the other hand, with the tendency of laser beam printers, digital copying apparatuses, etc. toward
20 compactness and lower cost, similar things are required of the scanning optical apparatus.

As an apparatus which makes these requirements compatible, a scanning optical apparatus in which the $f\theta$ lens is comprised of a single lens is variously
25 proposed, for example, in Japanese Patent Publication No. 61-48684, Japanese Laid-Open Patent Application No. 63-157122, Japanese Laid-Open Patent Application No.

4-104213, Japanese Laid-Open Patent Application No.
4-50908, etc.

Of these publications, in Japanese Patent
Publication No. 61-48684 and Japanese Laid-Open Patent
5 Application No. 63-157122, a concave single lens as on
f θ lens is used on the light deflector side to converge
a parallel beam of light from a collimator lens on the
surface of a recording medium. Also, in Japanese Laid-
Open Patent Application No. 4-104213, as f θ lenses, a
10 concave single lens and a toroidal-surfaced single lens
are used on the light deflector side and the image
plane side, respectively, to make a beam of light
converted into convergent light by a collimator lens
enter the f θ lenses. Also, in Japanese Laid-Open
15 Patent Application No. 4-50908, a single lens
introducing a high-order aspherical surface into a lens
surface is used as an f θ lens to make a beam of light
converted into convergent light by a collimator lens
enter the f θ lens.

20 However, in the scanning optical apparatuses
according to the prior art described above, according
to Japanese Patent Publication No. 61-48684, curvature
of image field in the sub scanning direction remains
and a parallel beam of light is imaged on the surface
25 to be scanned, and this has led to the problem that the
distance from the f θ lens to the surface to the scanned
becomes a focal length f and is long and it is

difficult to construct a compact scanning optical apparatus. In Japanese Laid-Open Patent Application No. 63-157122, the thickness of the $f\theta$ lens is great, and this has led to the problem that manufacture by molding is difficult and this makes a factor of increased cost. Japanese Laid-Open Patent Application No. 4-104213 has suffered from the problem that distortion remains. In Japanese Laid-Open Patent Application No. 4-50908, an $f\theta$ lens having a high-order aspherical surface is used and aberrations are corrected well, but there has been the problem that jitter of a period corresponding to the number of polygon surfaces occurs due to the mounting error of a polygon mirror which is a light deflector.

note!

Further, problems common to these $f\theta$ lenses each comprised of a single lens has included the problem that due to the non-uniformity of the lateral magnification in the sub scanning direction between the light deflector and the surface to be scanned, the spot diameter in the sub scanning direction changes depending on image height.

25
H2

Figures 2A and 2B of the accompanying drawings are cross-sectional views of the essential portions of a single beam scanning optical apparatus in the main scanning direction and the sub scanning direction, respectively, which apparatus has been proposed by the inventor in Japanese Patent Application No. 6-239386

6

(filed on September 6, 1994), and show changes in the spot diameter (F number) in the sub scanning direction due to image height. In these figures, the same elements as the elements shown in Figure 1 are given the same reference numerals.

Usually, in a plane inclination correcting optical system, it is necessary to bring the deflecting surface of a light deflector and a surface to be scanned into an optically conjugate relation (imaging relation) in order to optically correct the plane inclination of the deflecting surface. Accordingly, in an $f\theta$ lens having a predetermined lens shape in the main scanning section as in the aforescribed examples of the prior art, lateral magnification is high on the axis (on-axis beam 21) as indicated at (1) in Figure 2B, and lateral magnification becomes low off the axis (most off-axis beam 22) as indicated at (2) in Figure 2B (there is also a case where this becomes converse depending on the lens shape in the main scanning section).

Thus, irregularity occurs to the lateral magnification in the sub scanning direction depending on the lens shape of the $f\theta$ lens in the main scanning plane thereof and a change in the spot diameter in the sub scanning direction due to image height occurs.

On the other hand, the ability of higher speed scanning is required of a scanning optical apparatus for use in an LBP because of the tendency of the LBP

toward higher speed and higher accuracy, and from limitations such as the number of revolutions of a motor which is scanning means and the number of surfaces of a polygon mirror which is deflecting means, particularly the demand for a multibeam scanning optical apparatus capable of scanning a plurality of beams of light at a time is growing.

The above-described non-uniformity of the lateral magnification in the sub scanning direction makes the curve of the scanning line when the position of a light source (light source unit) is off the optical axis in Z direction indicated in Figures 2A and 2B and therefore, an optical system such as a multibeam scanning optical system (multibeam scanning optical apparatus) which scans a surface to be scanned at a time by the use of a plurality of beams of light off the optical axis has suffered from the problem that the scanning line bends on the surface to be scanned and as a result, the deterioration of image quality due to pitch irregularity occurs.

SUMMARY OF THE INVENTION

It is a first object of the present invention to provide a compact scanning optical apparatus suitable for highly accurate printing in which when a beam of light from a light source converted by a collimator lens or the like is to be imaged on a surface to be

scanned by an $f\theta$ lens through a light deflector, the lens shape (the main scanning plane shape) of the $f\theta$ lens in the main scanning plane thereof is optimized to thereby correct curvature of image field, distortion, etc. and the non-uniformity of lateral magnification in the sub scanning direction between the light deflector and the surface to be scanned is eliminated by only the lens shape (the sub scanning plane shape) in the sub scanning plane, independently of the lens shape in the main scanning plane, whereby any change in F number (F No.) in the sub scanning direction due to image height, i.e., any change in spot diameter, can be suppressed.

It is a second object of the present invention to provide a compact multibeam scanning optical apparatus suitable for highly accurate printing in which a plurality of beams of light from a light source converted by a collimator lens or the like is to be imaged on a surface to be scanned by an $f\theta$ lens through a light deflector, the lens shape (the main scanning plane shape) of the $f\theta$ lens in the main scanning plane thereof is optimized to thereby correct curvature of image field, distortion, etc. and the non-uniformity of lateral magnification in the sub scanning direction between the light deflection and the surface to be scanned is eliminated by only the lens shape (the sub scanning plane shape) in the sub scanning plane, independently of the lens shape in the main scanning

plane, whereby any change F number (F No.) in the sub scanning direction in spot diameter, can be suppressed and a beam of light from the light source which is off the optical axis in the sub scanning direction can also
5 be scanned highly accurately without the curve of the scanning line occurring.

The scanning optical apparatus of the present invention is

(1-1) a scanning optical apparatus in which a beam
10 of light emitted from light source means is imaged into a linear shape long in the main scanning direction on the deflecting surface of a deflecting element through a first optical element and a second optical element and the beam of light deflected by the deflecting
15 element is imaged into a spot-like shape on a surface to be scanned through a third optical element to thereby scan the surface to be scanned, characterized in that the third optical element comprise a single lens, the opposite lens surfaces of the single lens
20 both comprise a tori surface of an aspherical shape in the main scanning plane, and the curvature thereof in the sub scanning section is continuously varied from the on-axis toward the off-axis in the effective portion of the lens to thereby suppress any change of F
25 number in the sub scanning direction due to the image height of the beam of light incident on the surface to be scanned.

1 Particularly, it is characterized in
 (1-1-1) that the light source means has a plurality
of light source means has a plurality of light source
units capable of being independently modulated,

5 (1-1-2) that when the curve amounts of the loci, in
the main scanning plane, of the front side principal
plane and the rear side principal plane of the third
optical element in the sub scanning direction (the
difference in the direction of the optical axis between
10 the most off-axis principal plane position and the on-
axis principal plane position) are x_m and x_u ,
respectively, the following condition $x_m \leq dx \leq x_u$, is
satisfied:

where

15

$$dx = \frac{I_{pri} \cdot E_{pri} (\cos \theta_{img} - \cos \theta_{por})}{I_{pri} \cdot \cos \theta_{por} + E_{pri} \cdot \cos \theta_{img}}$$

I_{pri} : the distance from the deflecting surface
of the deflecting element in the on-axis
beam to the front side principal plane
in the sub scanning direction;

20 E_{pri} : the distance from the rear side
principal plane in the sub scanning
direction in the on-axis beam to the
surface to be scanned;

25 θ_{por} : the angle formed in the main scanning
plane by the most off-axis beam
deflected by the deflecting element with

T/10X

//

respect to the optical axis;

θ_{img} : the angle formed in the main scanning plane by the most off-axis beam incident on the surface to be scanned with respect to the optical axis;

5

(1-1-3) that the sign of the curvature of at least one of the opposite lens surfaces of the single lens constituting the third optical element in the subscanning plane is reversed from the on-axis toward the off-axis; and

10

(1-1-4) that the third optical element is made by plastic molding; or

(1-1-5) that the third optical element is made by glass molding.

15

The multibeam scanning optical apparatus of the present invention is

(2-1) a multibeam scanning optical apparatus in which a plurality of independently modulated beams of light emitted from light source means are imaged into linear shapes long in the main scanning direction on the deflecting surface of a deflecting element through a first optical element and a second element and the plurality of beams of light deflected by the deflecting element are imaged into a spot-like shape on a surface to be scanned through a third optical element to thereby scan the surface to be scanned,

20

25

characterized in that the third optical element

12

comprises a single lens, and the curvatures of the opposite lens surfaces of the single lens in the sub scanning direction are continuously varied from the on-axis toward the off-axis to thereby suppress any change of F number in the sub scanning direction due to the image height of the beam light incident on the surface to be scanned.

Particularly, it is characterized in

(2-1-1) that when the maximum value and minimum value of the F number of the beam of light incident on the surface to be scanned in the sub scanning direction are F_{\max} and F_{\min} , respectively, the curvatures of the opposite lens surfaces of the single lens constituting the third optical element in the sub scanning direction are continuously varied from the on-axis toward the off-axis so as to satisfy the condition that

$$F_{\min}/F_{\max} \geq 0.9,$$

(2-1-2) that the sign of the curvature of at least one of the opposite lens surfaces of the single lens constituting the third optical element in the sub scanning direction is reversed from the on-axis toward the off-axis,

(2-1-3) that the curvatures of the opposite lens surfaces of the single lens constituting the third optical element in the sub scanning direction are varied asymmetrically with respect to the optical axis from the on-axis toward the off-axis, and

(2-1-4) that the third optical element is made by plastic molding, or

(2-1-5) that the third optical element is made by glass molding.

5 (2-2) a multibeam scanning optical apparatus in which a plurality of independently modulated beams of light emitted from light source means are imaged into a linear shape long in the main scanning direction on the deflecting surface of a deflecting element through a
10 first optical element and a second optical element and the plurality of beams of light deflected by the deflecting element are imaged into a spot-like shape on a surface to be scanned through a third optical element is characterized in

15 that the third optical element is comprised of at least two lenses, and the curvatures of at least two lens surfaces of the two lenses in the sub scanning direction are continuously varied from the on-axis toward the off-axis to thereby suppress any change of F
20 number in the sub-scanning direction due to the image height of the beam of light incident on the surface to be scanned.

Particularly, it is characterized in

25 (2-2-1) that when the maximum value and minimum value of the F number of the beam of light incident on the surface to be scanned in the sub-scanning direction are F_{max} and F_{min} , respectively, the curvatures of at

least two lens surfaces of the two lenses constituting the third optical element in the sub scanning direction are continuously varied from the on-axis toward the off-axis so as to satisfy the condition that

5 $F_{min}/F_{max} \geq 0.9,$

(2-2-2) that the sign of the curvature of at least one lens surface of the two lenses constituting the third optical element in the sub scanning direction is reversed from the on-axis toward the off-axis,

10 (2-2-3) that the curvatures of at least two surfaces of the two lenses constituting the third optical element in the sub scanning direction are varied asymmetrically with respect to the optical axis from the on-axis toward the off-axis, and

15 (2-2-4) that at least one of the two lenses constituting the third optical element is made by plastic molding, or

(2-2-5) that at least one of the two lenses constituting the third optical element is made by glass
20 molding.

BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 is a schematic view of the essential portions of the optical system of a scanning optical
25 apparatus according to the prior art.

Figures 2A and 2B are cross-sectional views of the essential portions of the scanning optical apparatus

according to the prior art in the main scanning direction and the sub scanning direction, respectively.

Figure 3 is a cross-sectional view of the essential portions of a scanning optical apparatus
5 between a deflecting element and a surface to be scanned in the main scanning direction.

Figures 4A and 4B are cross-sectional views of the essential portions of Embodiment 1 of the present invention in the main scanning direction and the sub
10 scanning direction, respectively.

Figure 5 is an illustration showing the aspherical surface shape of an f θ lens in Embodiment 1 of the present invention.

Figure 6 is an illustration showing the shape of
15 the f θ lens in Embodiment 1 of the present invention in the main scanning direction.

Figure 7 is an illustration showing the defocus characteristic of a spot diameter in the sub scanning direction on a surface to be scanned in Embodiment 1 of
20 the present invention.

Figures 8A and 8B are cross-sectional views of the essential portions of Embodiment 2 of the present invention in the main scanning direction and the sub
scanning direction, respectively.

Figure 9 is an illustration showing the aspherical surface shape of an f θ lens in Embodiment 2 of the
25 present invention.

Figure 10 is an illustration showing the defocus characteristic of the spot diameter in the sub scanning direction on a surface to be scanned in Embodiment 2 of the present invention.

5 Figure 11 is an illustration showing the defocus characteristic of a spot diameter in the sub scanning direction on a surface to be scanned in Embodiment 2 of the present invention.

10 Figures 12A and 12B are cross-sectional views of the essential portions of Embodiment 3 of the present invention in the main scanning direction and the sub scanning direction, respectively.

15 Figure 13 is an illustration showing the aspherical surface shape of an $f\theta$ lens in Embodiment 3 of the present invention.

Figure 14 is an illustration showing the shape of the $f\theta$ lens in the main scanning direction in Embodiment 3 of the present invention.

20 Figure 15 is an illustration showing the curve of a scanning line in Embodiment 3 of the present invention.

25 Figures 16A and 16B are cross-sectional views of the essential portions of Embodiment 4 of the present invention in the main scanning direction and the sub scanning direction, respectively.

Figure 17 is an illustration showing a change in F number in the sub scanning direction on a surface to be

scanned relative to image height in Embodiment 4 of the present invention.

Figure 18 is an illustration showing the curvature of an $f\theta$ lens in the meridian-line direction relative to image height in Embodiment 4 of the present invention.

Figure 19 is an illustration showing the curvature of a scanning line during multibeam scanning at resolution 600 dpi (scanning line interval 42.3 μm) in Embodiment 4 of the present invention.

Figures 20A and 20B are cross-sectional views of the essential portions of Embodiment 5 of the present invention in the main scanning direction and the sub scanning direction, respectively.

Figure 21 is an illustration showing a change of F number in the sub scanning direction on a surface to be scanned relative to image height in Embodiment 5 of the present invention.

Figure 22 is an illustration showing the curvature of an $f\theta$ lens in the meridian-line direction relative to image height in Embodiment 5 of the present invention.

Figure 23 is an illustration showing the curve of a scanning line during multibeam scanning at resolution 600 dpi (scanning line interval 42.3 μm) in Embodiment 5 of the present invention.

Figures 24A and 24B are cross-sectional views of

the essential portions of Embodiment 6 of the present invention in the main scanning direction and the sub scanning direction, respectively.

Figure 25 is an illustration showing a change of F
5 number in the sub scanning direction on a surface to be scanned relative to image height in Embodiment 6 of the present invention.

Figure 26 is an illustration showing the curvature
of an f θ lens in the meridian-line direction relative
10 to image height in Embodiment 6 of the present invention.

Figure 27 is an illustration showing the curve of
a scanning line during multibeam scanning at resolution
600 dpi (scanning line interval 42.3 μ m) in Embodiment
15 6 of the present invention.

Figures 28A and 28B are cross-sectional views of
the essential portions in the main scanning direction
and the sub scanning direction, respectively, when
multibeam scanning was effected by the use of the
20 prior-art single beam scanning optical apparatus shown
in Figures 2A and 2B.

Figure 29 is an illustration showing a change of F
number in the sub scanning direction on a surface to be
scanned relative to image height in the single beam
25 scanning optical apparatus shown in Figures 28A and
28B.

Figure 30 is an illustration showing the curvature

of an $f\theta$ lens in the meridian-line direction relative to image height in the single beam scanning optical apparatus shown in Figures 28A and 28B.

5 Figure 31 is an illustration showing the curve of a scanning line during multibeam scanning at resolution 600 dpi (scanning line interval $42.3\ \mu\text{m}$) in the single beam scanning optical apparatus shown in Figures 28A and 28B.

10 DESCRIPTION OF THE PREFERRED EMBODIMENTS

Before some embodiments of the scanning optical apparatus of the present invention are described, means for achieving the objects of the present invention will first be described. To achieve the above-described
15 objects in the scanning optical apparatus, it is necessary to optimize the lens shape of the $f\theta$ lens and to uniformize the lateral magnifications in the sub scanning direction on the axis and off the axis.

Figure 3 is a cross-sectional view of the essential
20 portions in the main scanning direction between the light deflector (deflecting element) of the scanning optical apparatus and the surface to be scanned. To uniformize the lateral magnifications in the sub scanning direction on the axis and off the axis, it is
25 necessary to determine the principal plane position so that the ratios of the lengths of optical path on the axis and off the axis may be equal to each other.

Accordingly, the principal plane position of the $f\theta$ lens in the sub scanning direction is determined so as to satisfy the following conditions:

$$Ipri : Epri = Imar : Emar$$

5 $Ipri \cdot Emar = Epri \cdot Imar \quad \dots\dots(a)$

where

10 $Ipri$: the distance from the deflecting surface of the light deflector to the front side principal plane in the sub scanning direction in the on-axis beam;

$Epri$: the distance from the rear side principal plane in the sub scanning direction to the surface to be scanned in the on-axis beam;

15 $Imar$: the distance from the deflecting surface of the light deflector to the front side principal plane in the sub scanning direction in the most off-axis beam;

20 $Emar$: the distance from the rear side principal plane in the sub scanning direction to the surface to be scanned in the most off-axis beam.

25 Generally, the off-axis beam is refracted in the direction of the optical axis in the main scanning plane in order to satisfy the $f\theta$ characteristic and therefore, a focus 71 in the main scanning plane of the principal plane in the sub scanning direction for

satisfying the above expression (a) is a plane curved toward a light deflector 5 off the axis as shown in Figure 3. Here, when the curve amount on the most off-axis is dx,

5
$$E_{mar} = (E_{pri} + dx) / \cos \theta_{img}$$

$$I_{mar} = (I_{pri} - dx) / \cos \theta_{por}$$

and consequently,

$$I_{pri}(E_{pri} + dx) / \cos \theta_{img} = E_{pri}(I_{pri} - dx) / \cos \theta_{img}$$

$$dx(I_{pri} \cdot \cos \theta_{por} + E_{pri} \cdot \cos \theta_{img})$$

$$= I_{pri} \cdot E_{pri}(\cos \theta_{img} - \cos \theta_{por})$$

$$dx = \frac{I_{pri} \cdot E_{pri}(\cos \theta_{img} - \cos \theta_{por})}{I_{pri} \cdot \cos \theta_{por} + E_{pri} \cdot \cos \theta_{img}} \dots (b)$$

where

15 θ_{por} : the angle formed in the main scanning plane by the most off-axis beam deflected by the light deflector with respect to the optical axis of the $f\theta$ lens;

20 θ_{img} : the angle formed in the main scanning plane by the most off-axis beam incident on the surface to be scanned with respect to the optical axis of the $f\theta$ lens.

25 Accordingly, to uniformize the lateral magnification in the sub scanning direction, it is necessary to set the curve amount dx of the locus of the principal plane in the sub scanning direction to a

value derived from the above expression (b).

That is, when in an actual scanning optical apparatus, the curve amounts of the loci, in the main scanning plane, of the front side principal plane and the rear side principal plane of an $f\theta$ lens in the sub scanning direction (the difference in the direction of the optical axis between the most off-axis principal plane position and the on-axis principal plane position) are x_m and x_u , respectively, it is desirable to determine the principal plane position so as to satisfy the condition that

$$x_m \leq dx \leq x_u. \quad \dots\dots(1)$$

If the above conditional expression (1) is departed from, irregularity will occur to the lateral magnification in the sub scanning direction and the change in spot diameter due to image height will become great, and this will pose a problem in practice.

Next, as regards a method of changing the principal plane position in the sub scanning direction, the deflecting surface of the light deflector and the surface to be scanned are brought into optically conjugate relationship with each other in the sub scanning direction of the $f\theta$ lens as previously described to thereby effect the correction of plane inclination and therefore, the refractive power itself of the $f\theta$ lens cannot be varied.

Accordingly, the first lens surface (R_1 surface)

23

and the second lens surface (R2 surface) of the f θ lens in the sub scanning direction are bent to thereby effect the movement of the principal plane position. By the bending, the principal plane of the lens can be moved without the refractive power of the lens itself being changed and therefore, the meridian line r is continuously changed from the on-axis toward the off-axis and an optimum lens shape can be provided depending on location, whereby the lateral magnification in the sub scanning direction can be uniformized.

By optimizing the lens shape of the f θ lens in this manner, the F number (F No.) in the sub scanning direction of the beam of light incident on the surface to be scanned can be uniformized, and the variation in the spot diameter in the sub scanning direction due to image height which has heretofore been a problem peculiar to a single-lens f θ lens can be minimized.

Also for a beam of light emerging from a light source (light source unit) off the optical axis, the surface to be scanned can be highly accurately scanned without causing the curve of the scanning line, whereby there can be provided a scanning optical apparatus suitable also for multibeam scanning.

Some embodiments of the present invention will now be described.

Figures 4A and 4B are cross-sectional views of

24

Embodiment 1 of the present invention in the main scanning direction and the sub scanning direction, respectively.

In these figures, reference numeral 1 designates
5 light source means (a light source unit) comprising,
for example, a semiconductor laser.

Reference numeral 2 denotes a collimator lens as a
first optical element which converts a divergent beam
of light emitted from the light source means 1 into a
10 convergent beam of light. Reference numeral 3
designates an aperture stop which regularizes the
diameter of the beam of light passing therethrough.

Reference numeral 4 denotes a cylindrical lens as
a second optical element which has predetermined
15 refractive power only in the sub scanning direction and
causes the beam of light passed through the aperture
stop 3 to be imaged as a substantially linear image on
the deflecting surface 5a of a light deflector
(deflecting element) 5 which will be described later in
20 the sub scanning section.

Reference numeral 5 designates a light deflector
as a deflecting element which comprises, for example, a
polygon mirror (rotatable polygon mirror) and is
rotated at a predetermined speed in the direction of
25 arrow A by drive means (not shown) such as a motor.

Reference numeral 6 denotes an f θ lens (imaging
optical system) as a third optical element comprising a

lens having the $f\theta$ characteristic and disposed more toward the light deflector 5 side than the intermediate portion between the light deflector 5 and a photosensitive drum surface 8 as a surface to be scanned. In the present embodiment, the opposite lens surface of the $f\theta$ lens 6 both comprise a toric surface which is aspherical in the main scanning plane, and continuously varies the curvature in the sub scanning plane (a plane containing the optical axis of the third optical element and orthogonal to the main scanning plane) from the on-axis toward the off-axis in the effective portion of the lens. Thereby, in Embodiment 1, the change in F number (F No.) in the sub scanning direction due to the image height of the beam of light incident on the surface 8 to be scanned, i.e., the change in spot diameter, is minimized. The $f\theta$ lens 6 causes the beam of light based on image information deflected and reflected by the light deflector 5 to be imaged on the photosensitive drum surface 8 and corrects the plane inclination of the deflecting surface of the light deflector 5.

In Embodiment 1, the $f\theta$ lens 6 may be made by plastic molding or may be made by glass molding.

In Embodiment 1, the divergent beam of light emitted from the semiconductor laser 1 is converted into a convergent beam of light by the collimator lens 2, and this beam of light (the quantity of light) is

limited by the aperture stop 3 and enters the cylindrical lens 4. The beam of light having entered the cylindrical lens 4, in the main scanning section, emerges therefrom intactly in that state. Also, in the
5 sub scanning section, it converges and is imaged as a substantially linear image (a linear image long in the main scanning direction) on the deflecting surface 5a of the light deflector 5. The beam of light deflected and reflected by the deflecting surface 5a of the light
10 deflector 5 is directed onto the photosensitive drum surface 8 through the $f\theta$ lens 6 having different refractive powers in the main scanning direction and the sub scanning direction, and scans the photosensitive drum surface 8 in the direction of arrow
15 B by the light deflector 5 being rotated in the direction of arrow A. Thereby, image recording is effected on the photosensitive drum 8 which is a recording medium.

In Embodiment 1, the lens shape of the $f\theta$ lens in
20 the main scanning direction is an aspherical surface shape which can be represented by a function up to the tenth-order, and the lens shape in the sub scanning direction is comprised of a spherical surface continuously varying in the direction of image height.
25 The lens shape, when for example, the point of intersection between the $f\theta$ lens and the optical axis is the origin and the direction of the optical axis is

1 the X-axis and the axis orthogonal to the optical axis
in the main scanning plane is the Y-axis and the axis
orthogonal to the optical axis in the sub scanning
plane is the Z-axis, is such that the generating-line
5 direction corresponding to the main scanning direction
can be represented by the following expression:

$$X = \frac{Y^2/R}{1 + (1 - (1+K)(Y/R)^2)^{1/2}}$$

$$+ B_4 Y^4 + B_6 Y^6 + B_8 Y^8 + B_{10} Y^{10}, \quad \dots\dots(c)$$

(where R is the radius of curvature, K, B₄, B₆, B₈
and B₁₀ are aspherical surface coefficients)
and the meridian-line direction corresponding to the
sub scanning direction (the direction orthogonal to the
main scanning direction containing the optical axis)
15 can be represented by the following expression:

$$S = \frac{Z^2/r'}{1 + (1 - (Z/r')^2)^{1/2}}, \quad \dots\dots(d)$$

(where $r' = r(1 + D_2 Y^2 + D_4 Y^4 + D_6 Y^6 + D_8 Y^8 + D_{10} Y^{10})$).

20 Table 1 below shows the optical arrangement in
Embodiment 1 and the aspherical surface coefficients of
the fθ lens 6.

Table 1 (Embodiment 1)

wavelength used	λ (nm)	780	shape of f θ lens	
			1st surface	2nd surface
refractive index of f θ lens	n	1.519	R	6.7814E+01
angle of incidence on polygon	θ_i	-90	K	-1.6787E+01
maximum angle of emergence from polygon	θ_{max}	45	B4	-9.8604E-07
polygon - f θ lens	e	36	B6	1.5479E-11
center thickness of f θ lens	d	11	B8	8.7055E-14
f θ lens - surface to be scanned	Sk	110.5	B10	-4.7942E-18
maximum effective diameter of f θ lens	Ymax	42	r	-2.7332E+01
focal length of f θ lens	ft	213.7	D2S	1.2604E-03
degree of convergence of collimator polygon - natural converging point	fc	317.3	D4S	1.2255E-06
			D6S	8.4502E-10
			D8S	-6.3449E-13
			D10S	1.3148E-15
			D2E	9.3936E-04
			D4E	2.027E-06
			D6E	7.0546E-10
			D8E	-1.2936E-12
			D10E	2.3372E-15
				4.3944E-18

T290X

Figure 5 is an illustration showing a change of curvature in the sub scanning direction relative to the position of the f θ lens 6 in the lengthwise direction. As shown in Figure 5, the curvature of the meniscus shape is sharp on the axis and becomes plano-convex from the on-axis toward the off-axis. Figure 6 is an illustration showing the aspherical surface shape of the f θ lens 6. In Figure 6, thick solid lines indicate the lens surface shapes in the main scanning direction, and thin solid lines are the loci of the principal plane in the sub scanning direction, and indicate the front side principal plane and the rear side principal plane.

In Embodiment 1, the curve amount dx of the locus of the principal plane for suppressing the change of lateral magnification in the sub scanning direction due to image height is

$$dx = 6.50$$

from

$$Ipri = 48.73 \quad Epri = 108.77$$

$$\theta_{por} = 44.4^\circ \quad \theta_{img} = 29.10^\circ.$$

Also, the curve amount xm of the locus of the front side principal plane of the f θ lens 6 in the sub scanning direction and the curve amount xu of the locus of the rear side principal plane thereof are

$$xm = 3.24 \quad xu = 7.48$$

and these values satisfy the aforementioned conditional

expression (1) ($x_m \leq dx \leq x_u$).

Thereby, in Embodiment 1, the lateral magnification in the sub scanning direction between the light deflector 5 and the surface 8 to be scanned can be uniformized on the axis and off the axis to a level free of any practical problem, and as shown in Figure 7, the change of the spot diameter in the sub scanning direction due to image height can be minimized. Thereby, there is achieved a scanning optical apparatus which is inexpensive and suitable for highly accurate printing.

Figures 8A and 8B are cross-sectional views of Embodiment 2 of the present invention in the main scanning direction and the sub scanning direction, respectively. In Figures 8A and 8B, the same elements as the elements shown in Figures 4A and 4B are given the same reference numerals.

The differences of Embodiment 2 from the aforescribed Embodiment 1 are that the divergent beam of light emitted from the semiconductor laser (the light source unit) is converted not into a convergent beam of light but into a parallel beam of light by the collimator lens and that corresponding thereto, the lens shape of the $f\theta$ lens is made different. In the other points, the construction and optical action of Embodiment 2 are substantially similar to those of Embodiment 1, whereby a similar effect is obtained.

Table 2 below shows the optical arrangement in Embodiment 2 and the aspherical surface coefficients of an f θ lens 26.



Table 2 (Embodiment 2)

wavelength used	λ (nm)	shape of f θ lens		
			1st surface	2nd surface
refractive index of f θ lens	n	780	R	2.2000E+02
angle of incidence on polygon	θ_i	1.519	K	-1.1768E+02
maximum angle of emergence from polygon	θ_{max}	-60	B4	0.0000E+00
polygon - f θ lens	e	42	B6	-5.2353E-07
center thickness of f θ lens	d	40	B8	-8.6171E-11
f θ lens - surface to be scanned	Sk	15	B10	1.8432E-14
maximum effective diameter of f θ lens	Ymax	146.45	r	8.4808E-18
focal length of f θ lens	ft	43	d2S	-1.7832E+01
		150	d4S	4.5963E-05
			d6S	-7.1210E-08
			d8S	1.7390E-11
			d10S	-4.3029E-15
			d2E	-1.4545E-19
			d4E	1.1994E-05
			d6E	-5.9970E-08
			d8E	-1.7699E-12
			d10E	2.1846E-14
				-9.2552E-18

Figure 9 is an illustration showing a change of curvature in the sub scanning direction relative to the position of the f θ lens 26 in the lengthwise direction. As shown in Figure 9, the curvature of the meniscus shape becomes sharper from the on-axis toward the off-axis. Figure 10 is an illustration showing the aspherical surface shape of the f θ lens 26. In Figure 10, thick solid lines indicate the lens surface shape in the main scanning direction, and thin solid lines are the loci of the principal plane in the sub scanning direction, and indicate the front side principal plane and the rear side principal plane.

In Embodiment 2, the curve amount dx of the locus of the principal plane for suppressing the change of lateral magnification in the sub scanning direction due to image height is

$$dx = 7.60$$

from

$$Ipri = 53.94 \quad Epri = 147.51$$

$$\theta_{por} = 42.0^\circ \quad \theta_{img} = 24.57^\circ.$$

Also, the curve amount xm of the locus of the front side principal plane of the f θ lens 26 in the sub scanning direction and the curve amount xu of the locus of the rear side principal plane thereof are

$$xm = 7.34 \quad xu = 12.31$$

and these values satisfy the aforementioned conditional expression (1) ($xm \leq dx \leq xu$).

Thereby, in Embodiment 2, as in the aforescribed
embodiment 1, the lateral magnification in the sub
scanning direction between the light deflector 25 and
the surface 8 to be scanned can be uniformized on the
5 axis and off the axis to a level free of any practical
problem, and as shown in Figure 11, the change of the
spot diameter in the sub scanning direction due to
image height can be minimized. Thereby, there is
achieved a scanning optical apparatus which is
10 inexpensive and suitable for highly accurate printing.

In Embodiment 2, the divergent beam of light
emitted from the semiconductor laser 1 is converted
into a parallel beam of light by the collimator lens 2
as previously described and therefore, the jitter by
15 the light deflector is null, and the lens shape, in the
main scanning direction, of the lens surface R2
preponderantly creating the power in the sub scanning
direction is similar to the shape of the locus of the
principal plane for uniformizing the lateral
20 magnification and therefore, the lateral magnification
can be uniformized even if the change of curvature in
the meridian-line direction due to image height is
small, whereby there can be achieved a scanning optical
apparatus suitable for further highly accurate
25 printing.

Figures 12A and 12B are cross-sectional views of
Embodiment 3 of the present invention in the main

scanning direction and the sub scanning direction, respectively. In these figures, the same element as the elements shown in Figure 4 are given the same reference numerals.

5 The differences of Embodiment 3 from the
aforedescribed Embodiment 1 are that the apparatus is
comprised of a multibeam scanning optical system for
scanning a plurality of beams of light emitted from
light source means 11 having a plurality of (in
10 Embodiment 3, too) light source units capable of being
independently modulated, at a time, so as to have a
predetermined interval therebetween on the surface to
be scanned, and that correspondingly thereto, the lens
shape of the f θ lens in the meridian-line direction
15 (the sub scanning direction) is made different. In the
other points, the construction and optical action of
Embodiment 3 are substantially similar to those of the
aforedescribed Embodiment 1, whereby a similar effect
is obtained. The above-described plurality of light
20 source units are disposed at a predetermined interval
in the sub scanning direction.

Table 3 below shows the optical arrangement in
Embodiment 3 and the aspherical surface coefficients of
the f θ lens 36.

Table 3 (Embodiment 3)

wavelength used	λ (nm)	780	shape of f θ lens	
			1st surface	2nd surface
refractive index of f θ lens	n	1.519	R	6.7814E+01
angle of incidence on polygon	θ_i	-90	K	-1.6787E+01
maximum angle of emergence from polygon	θ_{max}	45	B4	-9.8604E-07
polygon - f θ lens	e	36	B6	1.5479E-11
center thickness of f θ lens	d	11	B8	8.7055E-14
f θ lens - surface to be scanned	Sk	110.5	B10	-4.7942E-18
maximum effective diameter of f θ lens	Ymax	42	r	-2.8363E+01
focal length of f θ lens	ft	213.7	d2S	5.4992E-05
degree of convergence of collimator polygon - natural converging point	fc	317.3	d4S	-2.2581E-08
			d6S	9.5892E-12
			d8S	-1.9648E-15
			d10S	2.7992E-19
			d2E	4.3102E-05
			d4E	1.7579E-08
			d6E	-3.6419E-11
			d8E	2.1285E-14
			d10E	-4.6427E-18
				8.2100E-20

1 In Embodiment 3, the lens shape of at least one of
the lens surfaces of the f θ lens 36 in the meridian-
line direction is set so that the sign of curvature may
be reversed from on the on-axis toward the off-axis.

5 Therefore, the meridian-line direction of the f θ lens
36 corresponding to the sub scanning direction is
represented by the following expression:

13807

$$S = \frac{Z^2/r'}{1 + (1 - (Z/r')^2)^{1/2}}, \quad \dots (e)$$

10 where $r' = r + d_2 Y^2 + d_4 Y^4 + d_6 Y^6 + d_8 Y^8 + d_{10} Y^{10}$. Also, the
generating-line direction corresponding to the main
scanning direction is represented by expression (c) as
in the aforescribed Embodiment 1.

15 Figure 13 is an illustration showing a change of
curvature in the sub scanning direction relative to the
position of the f θ lens 36 in Embodiment 3 in the
lengthwise direction. As shown in Figure 13, on the
lens surface R1, the sign of curvature in the sub
scanning direction is reversed from on the on-axis
20 toward the off-axis, and the meniscus shape on the axis
changes into a biconvex shape off the axis. Figure 14
is an illustration showing the aspherical surface shape
of the f θ lens 36. In Figure 14, thick solid lines
indicate the lens surface shape in the main scanning
25 direction, and thin solid lines are the loci of the
principal plane in the sub scanning direction, and
indicate the front side principal plane and the rear

side principal plane.

In Embodiment 3, the curve amount dx of the locus of the principal plane for suppressing the change of lateral magnification in the sub scanning direction due to image height is

$$dx = 6.50$$

from

$$P_{pri} = 48.73 \quad E_{pri} = 108.77$$

$$\theta_{por} = 44.4^\circ \quad \theta_{img} = 29.10^\circ.$$

Also, the curve amount x_m of the locus of the front side principal plane of the $f\theta$ lens 36 in the sub scanning direction and the curve amount x_u of the locus of the rear side principal plane thereof are

$$x_m = 4.93 \quad x_u = 9.10$$

and these values satisfy the aforementioned conditional expression (1) ($x_m \leq dx \leq x_u$).

Thus, in Embodiment 3, as in the aforescribed Embodiments 1 and 2, the lateral magnification in the sub scanning direction between the light deflector 5 and the surface 8 to be scanned can be uniformized to a level free of any practical problem on the axis and off the axis, and the change of the spot diameter in the sub scanning direction due to image height can be minimized. Thereby, there is achieved a scanning optical apparatus which is inexpensive and suitable for highly accurate printing.

Also, Embodiment 3 is a multibeam scanning optical

apparatus using a plurality of beams of light to scan the surface to be scanned at a time and therefore, the curve of the scanning line provides pitch irregularity on the image and this is not good.

5 So, in Embodiment 3, the radius of curvature in the sub scanning direction is continuously varied in the effective portion of the lens by image height, whereby the curve of the scanning line on the surface to be scanned can be eliminated as shown in Figure 15,
10 and thus, there is achieved a scanning optical apparatus (multibeam scanning optical apparatus) of high image quality free of pitch irregularity.

 Figures 16A and 16B are cross-sectional views of the essential portions of Embodiment 4 of the present
15 invention in the main scanning direction and the sub scanning direction, respectively. In these figures, the same element as the elements shown in Figures 12A and 12B are given the same reference numerals.

 In Figures 16A and 16B, reference numeral 46
20 designates an f θ lens (an imaging optical system) comprising a lens having the f θ characteristic as a third optical element, and this f θ lens 46 is disposed more toward the light deflector 5 than the intermediate portion between the light deflector 5 and the
25 photosensitive drum surface 8 as the surface to be scanned.

 In Embodiment 4, the opposite lens surfaces of the

f θ lens 46 both have their curvatures in the sub scanning direction continuously varied from the on-axis f θ lens 46 both have their curvatures in the sub scanning direction continuously varied from the on-axis toward the off-axis. Thereby, in Embodiment 4, the change of F number in the sub scanning direction due to the image height of the beam of light incident on the surface to be scanned, i.e., the change of the spot diameter, is minimized. Also, the sign of the curvature of at least one (the first surface) R1 of the opposite lens surfaces of the f θ lens 46 in the sub scanning direction is reversed from the on-axis toward the off-axis. Further, the curvatures of the opposite lens surfaces of the f θ lens in the sub scanning direction are varied from the on-axis toward the off-axis so as to become asymmetrical with respect to the optical axis. The f θ lens 46 causes a plurality of beams of light based on image information deflected and reflected by the light deflector 5 to be imaged on the photosensitive drum surface 8 and corrects the plane inclination of the deflecting surface of the light deflector 5.

In Embodiment 4, the f θ lens 46 may be made by plastic molding or may be made by glass molding.

In Embodiment 4, two independently modulated divergent beams of light emitted from a semiconductor laser 11 are converted into convergent beams of light

41

by the collimator lens 2, and these beams of light (the quantity of light) are limited by the aperture stop 3 and enter the cylindrical lens 4. The beams of light having entered the cylindrical lens 4, in the main scanning section, emerge therefrom intactly in that state. Also, in the sub scanning section, they converge and are imaged as substantially linear images (linear images long in the main scanning direction) on the deflecting surface 5a of the light deflector 5.

10 The two beams of light deflected and reflected by the deflecting surface 5a of the light deflector 5 from two spots on the photosensitive drum surface 8 through the f θ lens 46 having different refractive powers in the main scanning direction and the sub scanning direction,

15 and scan the photosensitive drum surface 8 in the direction of arrow B by the light deflector 5 being rotated in the direction of arrow A. Thereby, image recording is effected.

In Embodiment 4, the lens shape of the f θ lens 46, in the main scanning direction, is made into an aspherical surface shape capable of being represented by a function up to the 10th order in the main scanning direction and in the sub scanning direction, is comprised of a spherical surface continuously varying

25 in the image height direction. That lens shape is such that the generating-line direction corresponding to the main scanning direction is indicated by the

aforementioned expression (c) and the meridian-line direction corresponding to the sub scanning direction (the direction orthogonal to the main scanning direction containing the optical axis of the f θ lens) can be represented by

7430X

$$S = \frac{Z^2/r'}{1 + (1 - (Z/r')^2)^{1/2}}, \quad \dots(f)$$

(where $1/r' = 1/r + D_2Y^2 + D_4Y^4 + D_6Y^6 + D_8Y^8 + D_{10}Y^{10}$).

Generally, in a multibeam scanning optical apparatus, to make pitch irregularity visually inconspicuous, it is desirable that the pitch irregularity due to the curve of the scanning line be 1/10 of the beam pitch in the sub scanning direction or less. For example, in the case of a scanning optical apparatus in which the resolution in the sub scanning direction is 600 dpi, the beam pitch in the sub scanning direction is 42 μm and therefore, allowable pitch irregularity is about 4 μm or less.

So, in Embodiment 4, when the maximum value and the minimum value of the F number of the beam of light incident on the surface to be scanned in the sub scanning direction are Fmax and Fmin, respectively, the curvatures of the opposite lens surfaces of the f θ lens 46 in the sub scanning direction are continuously varied from the on-axis toward the off-axis so as to satisfy the condition that

$$F_{\min}/F_{\max} \geq 0.9, \quad \dots(2)$$

43

whereby the curve of the scanning line can be eliminated to thereby achieve a multibeam scanning optical apparatus which suffers little from pitch irregularity and is high in image quality and compact.

5 If the above-mentioned condition is departed from, pitch irregularity will become visually conspicuous due to the curve of the scanning line and this will pose a problem in practice.

10 Table 4 below shows the optical arrangement in Embodiment 4 and the aspherical surface coefficients of the f θ lens 46.

Table 4 (Embodiment 4)

Design Data				shape of f θ lens	
		λ (nm)		1st surface	2nd surface
wavelength used			780	R	1.6154E+02
refractive index of f θ lens		n	1.519	K	-1.0814E+02
angle of incidence on polygon		θ_i	-90	B4	-2.2909E-06
maximum angle of emergence from polygon		θ_{max}	45	B6	7.1426E-10
polygon - f θ lens		e	36	B8	-3.2030E-13
center thickness of f θ lens		d	11	B10	7.9836E-17
f θ lens - surface to be scanned		Sk	110.5	r	-1.1966E+01
maximum effective diameter of f θ lens		Ymax	42	D2S	4.4462E-05
focal length of f θ lens		ft	213.7	D4S	-2.7866E-08
degree of convergence of collimator				D6S	2.5295E-11
polygon - natural converging point		fc	317.3	D8S	-1.0163E-14
polygon		circumscribed circle $\phi 20.4$ surfaces		D10S	1.9816E-18
				D2E	3.9194E-05
				D4E	-1.2704E-08
				D6E	1.1605E-11
				D8E	-3.3827E-15
				D10E	8.2100E-20

45

T450X

Figure 17 is an illustration showing a change of F number in the sub scanning direction on the surface to be scanned in Embodiment 4. In Embodiment 4, the curvatures of the f θ lens 46 in the sub scanning direction are continuously varied on the opposite lens surfaces from the on-axis toward the off-axis as shown in Figure 18 to thereby suppress the rate of change of F number due to image height so as to be

$$F_{\min}/F_{\max} = 64.52/66.31 = 0.973,$$

i.e., 0.9 or greater.

Figure 19 is an illustration showing the curve of the scanning line when the multibeam scanning optical apparatus of Embodiment 4 is used at resolution 600 dpi (scanning line interval 42.3 μ m). By suppressing the change of F number due to image height as described above, the curve of the scanning line can be brought to a level of the order of 0.2 μ m (pitch irregularity being of the order of 0.4 μ m) which is quite free of a practical problem.

Thus, in Embodiment 4, as described above, conditional expression (2) is satisfied and yet the curvatures of the f θ lens 46 in the sub scanning direction (the meridian-line direction) are continuously varied from the on-axis toward the off-axis to thereby suppress the change of F number in the sub scanning direction due to image height, i.e., the change of the spot diameter, to below a predetermined

amount (within the allowable value of the apparatus) and eliminate the pitch irregularity due to the curve of the scanning line which poses a problem in the multibeam scanning optical apparatus. Also, in

5 Embodiment 4, the third optical element ($f\theta$ lens) 46 is comprised of a single lens and therefore, there can be achieved a compact and low-cost multibeam scanning optical apparatus.

10 Figures 20A and 20B are cross-sectional views of the essential portions of Embodiment 5 of the present invention in the main scanning direction and the sub scanning direction, respectively. In these figures, the same elements as the elements shown in Figures 12A and 12B are given the same reference numerals.

15 The differences of Embodiment 5 from the
aforedescribed Embodiment 4 are that in order to make curvature of image field in the main scanning direction small so as to be capable of coping with further highly accurate printing, the curvatures of the opposite lens
20 surfaces of an $f\theta$ lens 56 in the generating-line direction are set so as to be asymmetrical with the optical axis, and that the number of the polygon surfaces of the polygon mirror 15 is changed from four to six to thereby cope with high-speed printing. In
25 the other points, the construction and optical action of Embodiment 5 are substantially similar to those of Embodiment 4, whereby a similar effect is obtained.

Table 5 below shows the optical arrangement in Embodiment 5 and the aspherical surface coefficients of the f θ lens 56.

Table 5 (Embodiment 5)

Design Data				shape of f θ lens	
		λ (nm)		1st surface	2nd surface
wavelength used		780	R	7.6014E+01	1.8577E+02
refractive index of f θ lens		1.524	K	-1.4188E+01	-9.3624E+01
angle of incidence on polygon		-60	B4S	-8.8268E-07	-1.6683E-06
maximum angle of emergence from polygon		41.0	B6S	8.8566E-11	3.5647E-10
polygon - f θ lens		41.1	B8S	4.0586E-14	-1.2120E-13
center thickness of f θ lens		10.4	B10S	-5.2861E-19	3.5062E-17
f θ lens - surface to be scanned		122.5	B4E	-8.8268E-07	-1.6683E-06
maximum effective diameter of f θ lens		42	B6E	5.2038E-11	3.5647E-10
focal length of f θ lens		237.7	B8E	6.4399E-14	-1.2120E-13
degree of convergence of collimator			B10E	-5.1518E-18	3.5062E-17
polygon - natural converging point		339.69	r	-3.0459E+01	-1.3017E+01
polygon		circumscribed circle ϕ 40 6 surfaces	D2S	-3.2380E-05	-1.4111E-06
			D4S	7.6080E-08	1.0715E-09
			D6S	-3.4870E-11	1.7648E-11
			D8S	5.0570E-15	-8.2750E-15
			D10S	0.0000E+00	1.0082E-18
			D2E	-3.5200E-05	-1.4111E-06
			D4E	8.0516E-08	1.0715E-09
			D6E	-3.8015E-11	1.7648E-11
			D8E	6.0665E-15	-8.2750E-15
			D10E	-1.1908E-19	1.0082E-18

T490X

49

Figure 21 is an illustration showing a change of F number in the sub scanning direction on the surface to be scanned in Embodiment 5. In Embodiment 5, the curvatures of the f θ lens 56 in the sub scanning direction are continuously varied on the opposite lens surfaces from the on-axis toward the off-axis as shown in Figure 22, to thereby suppress the rate of change of F number due to image height so as to be

$$F_{\min}/F_{\max} = 49.75/53.08 = 0.937,$$

i.e., 0.9 or greater.

Figure 23 is an illustration showing the curve of the scanning line when the multibeam scanning optical apparatus of Embodiment 5 is used at resolution 600 dpi (the scanning line interval 42.3 μ m). By suppressing the change of F number due to image height as described above, the curve of the scanning line can be brought to a level of the order of 1.2 μ m (the pitch irregularity being of the order of 2.4 μ m) quite free of a practical problem.

Thus, again in Embodiment 5, as in Embodiment 4, conditional expression (2) is satisfied and yet the curvatures of the opposite lens surfaces of the f θ lens 56 in the sub scanning direction (the meridian-line direction) are continuously varied from the on-axis toward the off-axis to thereby suppress the change of F number in the sub scanning direction due to image height, i.e., the change of the spot diameter, to below

a predetermined amount, and eliminate the pitch irregularity due to the curve of the scanning line which poses a problem in the multibeam scanning optical apparatus. Also, in Embodiment 5, the curvatures of the opposite lens surfaces of the $f\theta$ lens (the third optical element) 56 in the generating-line direction are set so as to be asymmetrical with respect to the optical axis to thereby suppress the curvature of image field in the main scanning direction and achieve a multibeam scanning optical apparatus suitable for further highly accurate printing.

Figures 24A and 24B are cross-sectional views of the essential portions of Embodiment 6 of the present invention in the main scanning direction and the sub scanning direction, respectively. In these figures, the same element as the elements shown in Figures 12A and 12B are given the same reference numerals.

The differences of Embodiment 6 from the aforescribed Embodiment 4 are that an $f\theta$ lens (the third optical element) 76 is comprised of two lenses and the pitch irregularity due to the curve of the scanning line is reduced at higher accuracy, that the beam of light from a semiconductor laser 11 having a plurality of light emitting portions capable of being independently modulated is converted into a substantially parallel beam of light by the collimator lens 2, and that the number of the polygon surfaces of

51

the polygon mirror 15 is changed from four to six to thereby cope with high-speed printing. In the other points, the construction and optical action of Embodiment 6 are substantially similar to those of the
5 aforedescribed Embodiment 4, whereby a similar effect is obtained.

That is, in Figures 24A and 24B, reference numeral 76 designates an $f\theta$ lens as a third optical element, which comprises two lenses, i.e., a spherical lens
10 (glass spherical lens) 76a as a first $f\theta$ lens formed of a glass material, and a toric lens (aspherical plastic toric lens) 76b as a second $f\theta$ lens of an aspherical surface shape formed of a plastic material. The glass
15 spherical lens 76a is disposed more toward the light deflector 15 than the intermediate portion between the light deflector 15 and the photosensitive drum surface 8 and has the function of correcting chiefly the $f\theta$ characteristic. The aspherical plastic toric lens 76b effects chiefly the correction of curvature of image
20 field and the correction of lateral magnification in the sub scanning direction.

In Embodiment 6, the curvatures, in the meridian-line direction (the sub scanning direction), of the opposite lens surfaces of the aspherical plastic toric
25 lens 76b bearing almost all of the refractive power in the sub scanning direction are continuously varied from the on-axis toward the off-axis to thereby suppress the

52

change of F number in the sub scanning direction on the surface to be scanned, i.e., the change of the spot diameter.

5 Table 6 below shows the optical arrangement in Embodiment 6 and the aspherical surface coefficients of the f θ lens (spherical lens 76a and toric lens 76b) 76.

TS40X

Table 6 (Embodiment 6)

Design Data				shape of 1st f θ lens	
wavelength used	λ (nm)			1st surface	2nd surface
refractive index of 1st f θ lens	n1	780		∞	-1.2042E+02
refractive index of 2nd f θ lens	n2	1.786		∞	-1.2042E+02
angle of incidence on polygon	θ 1	1.572		shape of 2nd f θ lens	
maximum angle of emergence from polygon	θ max	65		1st surface	2nd surface
polygon - 1st f θ lens	e1	45		-8.7734E+02	-3.4387E+02
center thickness of 1st f θ lens	d1	25.28		0.0000E+00	0.0000E+00
focal length of 1st to 2nd f θ lens	e2	14.00		-1.5203E-08	6.2830E-0.8
center thickness of 2nd f θ lens	d2	17.60		-1.2062E-11	-1.5527E-11
f θ lens - surface to be scanned	Sk	5.10		-1.2218E+01	-9.9689E+00
maximum effective diameter of f θ lens	Ymax	116.13		-4.2145E-07	4.2877E-07
focal length of f θ lens	ft	50		1.3072E-10	-7.9350E-10
polygon	circumscribed circle ϕ 40 6 surfaces	136		6.7762E-13	7.0965E-13
				D2E	1.2975E-07
				D4E	-2.2874E-10
				D6E	4.3863E-13

54

Figure 25 is an illustration showing a change of F number in the sub scanning direction on the surface to be scanned in Embodiment 6. In Embodiment 6, the curvatures of the toric lens 76b in the sub scanning direction are continuously varied on the opposite lens surfaces thereof from the on-axis toward the off-axis as shown in Figure 26 to thereby suppress the rate of change of F number due to image height so as to be

$$F_{min}/F_{max} = 72.67/73.75 = 0.985,$$

i.e., 0.9 or greater.

Figure 27 is an illustration showing the curve of the scanning line when the multibeam scanning optical apparatus of Embodiment 6 is used at resolution 600 dpi (scanning line interval 42.3 μ m). By suppressing the change of F number due to image height, the curve of the scanning line can be brought to a level of the order of 0.1 μ m (pitch irregularity being of the order of 0.2 μ m) free of a practical problem.

Thus, again in Embodiment 6, as in the aforedescribed Embodiment 4, conditional expression (2) is satisfied and yet the curvatures of the opposite lens surfaces of the toric lens 76b constituting the f θ lens 76 in the sub scanning direction (the meridian-line direction) are continuously varied from the on-axis toward the off-axis to thereby suppress the change of F number in the sub scanning direction due to height, i.e., the change of the spot diameter, to below

a predetermined amount and eliminate the pitch irregularity due to the curve of the scanning line which poses a problem in the multibeam scanning optical apparatus. Also, in Embodiment 6, by the $f\theta$ lens (the
5 third optical element) 76 being comprised of two lenses, the curve of the scanning line can be corrected more highly accurately, and there is achieved a multibeam scanning optical apparatus suitable for further highly accurate printing.

10 The sign of the curvature of at least one of the two lenses constituting the third optical element in the sub scanning direction may be reversed from the on-axis toward the off-axis, and the curvatures of at least two lens surfaces of the two lenses in the sub
15 scanning direction may be varied asymmetrically with respect to the optical axis from the on-axis toward the off-axis. Thereby, there can be achieved a multibeam scanning optical apparatus more suitable for highly accurate printing.

20 Lastly, for the comparison with the scanning optical apparatus of the present invention, description will be made of the manner in which multibeam scanning was effected by the prior-art single beam scanning optical apparatus shown in Figures 2A and 2B.

25 Figures 28A and 28B are cross-sectional views of the essential portions in the main scanning direction and the sub scanning direction, respectively, when

Sub 7
H3

Sub 7
H4
J6

multibeam scanning was effected by the use of the prior-art single beam scanning optical apparatus shown in Figures 2A and 2B, and show the changes of the angular magnification in the sub scanning direction and the spot diameter (F number) in the sub scanning direction on the surface to be scanned, due to image height. Table 7 below shows the optical arrangement shown in Figures 28A and 28B and the aspherical surface coefficients of an f θ lens 86.

Table 7

Design Data				shape of f θ lens	
		λ (nm)		1st surface	2nd surface
wavelength used		780		R	1.6154E+02
refractive index of f θ lens		n	1.519	K	-1.0814E+02
angle of incidence on polygon		θ_i	-90	B4	-2.2909E-06
maximum angle of emergence from polygon		θ_{max}	45	B6	7.1426E-10
polygon - f θ lens		e	36	B8	-3.2030E-13
center thickness of f θ lens		d	11	B10	7.9836E-17
f θ lens - surface to be scanned		Sk	110.5	r	-1.1991E+01
maximum effective diameter of f θ lens		Ymax	42	D2S	2.1635E-05
focal length of f θ lens		ft	213.7	D4S	-3.6548E-08
degree of convergence of collimator				D6S	2.7926E-11
polygon - natural converging point		fc	317.3	D8S	-1.1184E-14
polygon	circumscribed circle ϕ 20 4 surfaces			D10S	1.7618E-18
				D2E	2.2817E-05
				D4E	-3.8012E-08
				D6E	2.9368E-11
				D8E	-1.2060E-14
				D10E	1.9700E-18

In Figures 28A and 28B, two independently modulated divergent beams of light emitted from light source means 81 are converted into convergent beams of light by a collimator lens 82, and these beams of light (the quantity of light) are limited by a stop 83 and enter a cylindrical lens 84 having predetermined refractive power. The beams of light having entered the cylindrical lens 84, in the main scanning plane, intactly emerge in that state. Also, in the sub scanning section, they converge and are imaged as substantially linear images on the deflecting surface (reflecting surface) 85a of a light deflector 85 comprising a rotatable polygon mirror. The two beams of light deflected and reflected by the deflecting surface 85a of the light deflector 85 are directed onto a photosensitive drum surface as a surface 88 to be scanned through an imaging optical system ($f\theta$ lens) 86 having the $f\theta$ characteristic, and the light deflector 85 is rotated in the direction of arrow A, whereby the photosensitive drum surface 88 is light-scanned to thereby effect the recording of image information.

Usually, in a plane inclination correcting optical system, as previously described, it is necessary to bring the deflecting surface of the light deflector and the surface to be scanned into optically conjugate relationship (imaging relationship) with each other in order to optically correct the plane inclination of the

deflecting surface. In the comparative example shown in Figures 28A and 28B, with the curvature in the sub scanning direction (meridian line curvature) of that lens surface (first surface) R1 of the f θ lens 86 which is adjacent to the light deflector 85 being constant, the curvature in the sub scanning direction (meridian line curvature) of that lens surface (second surface) R2 of the f θ lens 86 which is adjacent to the surface to be scanned is continuously varied from the on-axis toward the off-axis to thereby bring about conjugate relationship at any image height.

However, the f θ lens 86 in the above-described comparative example is constant in the meridian line curvature of one surface (surface R1) thereof as shown in Figure 30 and therefore, as shown in Figure 29, depending on the bus line shape thereof, F number (F No) becomes irregular due to image height. That is, on the axis (the on-axis beam), the F number in the sub scanning direction on the surface to be scanned is great as shown in (1) in Figure 28B and therefore, the angular magnification in the sub scanning direction is small, and off the axis (the off-axis beam), the F number in the sub scanning direction is small as shown in (2) in Figure 28B and therefore, the angular magnification is great (there is a converse case depending on the main scanning plane shape).

Generally, between the angular magnification γ and

the lateral magnification β , the relation that

$$\beta\gamma = -1$$

is established and therefore, in the above-described comparative example, the lateral magnification becomes great on the axis and the lateral magnification becomes small off the axis. Therefore, due to image height, irregularity is created in the lateral magnification in the sub scanning direction, and in an optical system like a multibeam scanning optical apparatus which uses a plurality of laser beams off the optical axis to scan, the scanning line makes a curve on the surface to be scanned.

Figure 31 is an illustration showing the curve of the scanning line when the multibeam scanning optical apparatus of the comparative example is used at resolution 600 dpi (scanning line interval $42.3\mu\text{m}$). In Figure 31, the scanning line in the marginal portion is curved by $2.4\mu\text{m}$ with respect to the central portion, and this leads to the problem that pitch irregularity of $4.8\mu\text{m}$ will result and deteriorate the quality of image.

The above-noted problem does not arise in the scanning optical apparatus of the present invention, and according to a first invention, there can be achieved a compact scanning optical apparatus suitable for highly accurate printing in which when as previously described, a beam of light from a light

source converted by a collimator lens or the like is to be imaged on a surface to be scanned by an $f\theta$ lens through a light deflector, curvature of image field, distortion, etc. are well corrected by optimizing the lens shape of the $f\theta$ lens and the non-uniformity of the lateral magnification in the sub scanning direction between the light deflector and the surface to be scanned can be eliminated to thereby suppress the change of F number in the sub scanning direction due to image height, i.e., the change of the spot diameter.

Also, according to a second invention, there can be achieved a multibeam scanning optical apparatus in which when as previously described, a plurality of beams of light from a light source converted by a collimator lens or the like are to be imaged on a surface to be scanned by an $f\theta$ lens through a light deflector, curvature of image field, distortion, etc. are well corrected by optimizing the lens shape of the $f\theta$ lens and the non-uniformity of the lateral magnification in the sub scanning direction between the light deflector and the surface to be scanned can be eliminated to thereby suppress the change of F number in the sub scanning direction due to image height, i.e., the change of the spot diameter, and reduce the pitch irregularity due to the curve of the scanning line.

Further, there can be achieved a multibeam

scanning optical apparatus in which the curvature of
the $f\theta$ lens in the sub scanning direction is determined
so as to satisfy the aforementioned conditional
expression (2), whereby pitch irregularity can be
5 reduced to a visually problem-free level.